

# Removal and Replacement of Failed Bonded Nutplates Utilizing Nonmetallic Torlon® Adhesive Cutters



*Integrity ★ Service ★ Excellence*

**SAMPE**

**24 May 2018**

**Brett Bolan  
Paul Childers\*  
Jim Mazza  
AFRL/RXSA**

**Systems Support Division  
Materials & Manufacturing Directorate  
Air Force Research Laboratory**

*\*University of Dayton Research Institute*

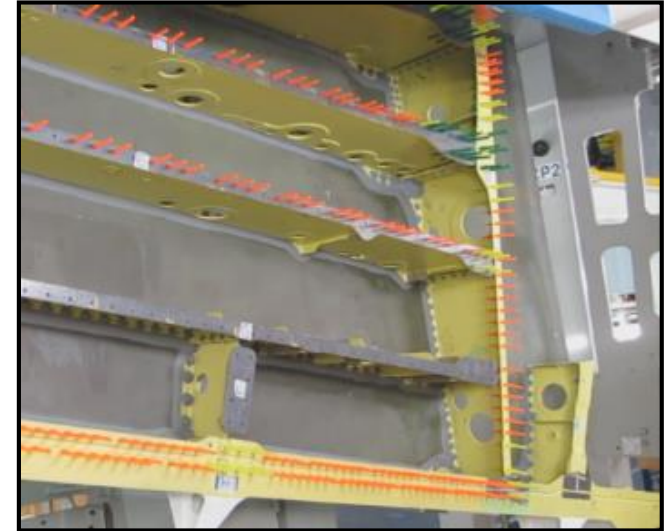


# Introduction

Adhesively bonded nutplates in manufacture of composite aerospace structures increasing (tens of thousands for some aircraft)

Utilized when two sided access not possible  
and/or maintenance access panels

- reducing # of holes
- reducing stress concentrations
- reducing installation & production costs
- reducing weight and rework



Operational units – nutplates that tend to fail are those used to secure panels and covers as they are frequently accessed (removed and reinstalled)



# Failed Nutplates

Nutplates fail for a variety of reasons



- poor surface prep



- wrong grip length fastener (too long) when engaged pushing nutplate off structure



- fastener locked up in nut element (i.e. not turning) due to excessive heat from fastener during installation



- Improper fastener torque sequencing for panel installation

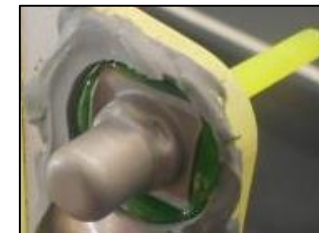
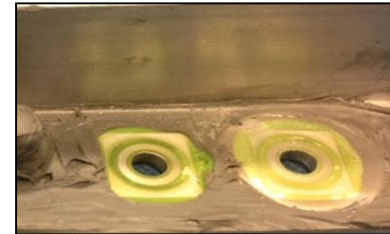
Following aircraft specific T.O. – takes from 24 to 72 hrs to effect a repair



# Replacement of Failed Nutplate



- Removal of residual sealant/adhesive
- Failed nutplate location properly prep'd for bonding
- Preparing faying surface of nutplate
- Verifying faying surfaces readiness/acceptability for bonding
- Reinstalling nutplate with 2-part adhesive

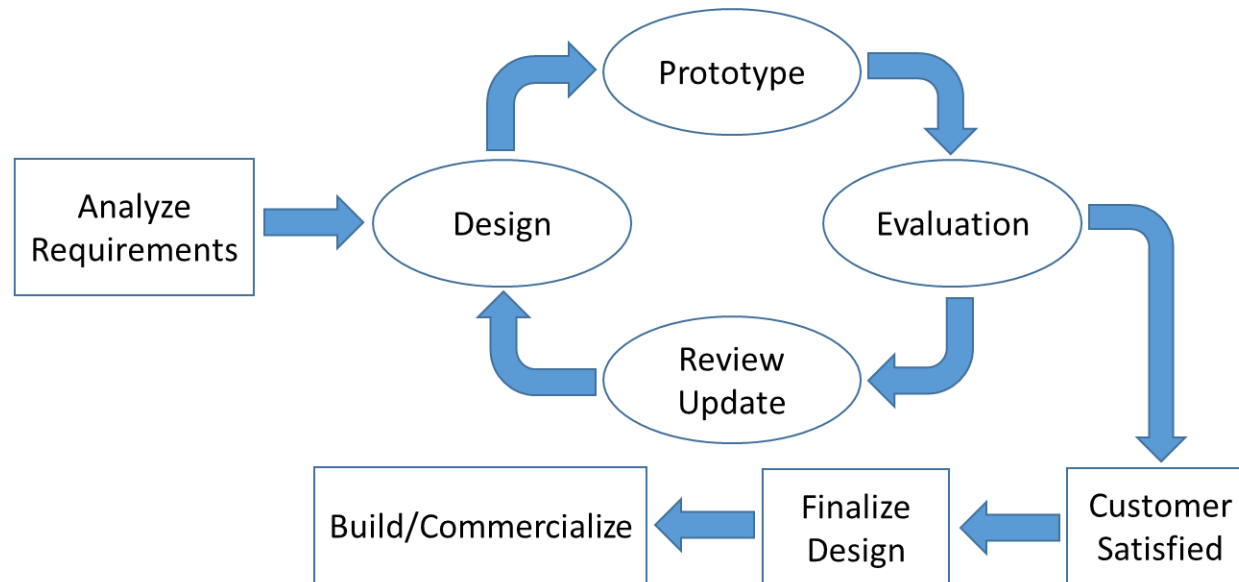


All steps in removal & replacement of a failed nutplate are important to returning aircraft to operational status - AFRL working with OEM to address  
Focus of this effort: reducing time to remove residual sealant/adhesive from hrs to min



# New Product Development Cycle

Iterative process followed to develop new removal tool  
multiple efforts conducted in parallel to reduce time to deliver final product



## Key - Analyzing Requirements

Comprehensive understanding of end-user requirements (OEM and aircraft operational units)  
Multiple site visits: discussions with OEM, Field Service Engineers, technicians & maintainers

Tool to be used in an operational environment  
Needs to access most failed nutplate locations (target 90% or greater)  
Rapidly prepare structure for a new nutplate w/o damaging underlying structure



# Operational Units

## Survey of Current Practices



Current T.O. authorized plastic removal tools

- did not adequately perform function
- time consuming



Led to (in some instances):



Use of non-authorized metallic removal tools

- removed sealant/adhesive quickly
- high potential to damage structure  
scratches and gouges – extensive rework





# OEM Production

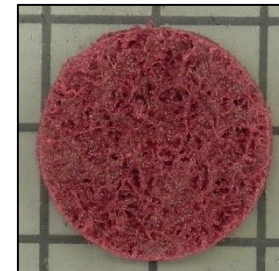
## Survey of Current Practices

Early in the manufacturing process better access to aircraft structure

– subsystems & hardware not installed

Nutplate failures further down the manufacturing line or on the flight-line

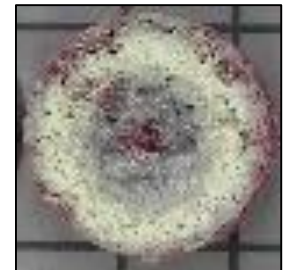
- similar challenges to operational units (restricted access)



Norton Vortex  
Medium Pad

Using a 3200 rpm pneumatic rotary tool with an abrasive pad to remove sealant/adhesive – heat generated causes sealant/adhesive to smear on faying surface and rapidly clogs pads

- 10 or more pads required to achieve clean surface
- access limited by throat depth
- cannot be used on composites





# Design: Prototype Development



Determine if a Torlon scraper blade developed for another program is viable for this application



Attach 5030 glass-filled Torlon blade to a pneumatic driven tool to remove adhesive from a composite panel



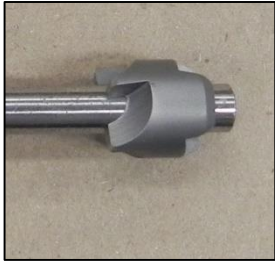
Easily removes adhesive with no visible damage to underlying structure

Field trials demonstrated inability to access many locations due to tools bulkiness  
- does not meet “accessibility” requirement



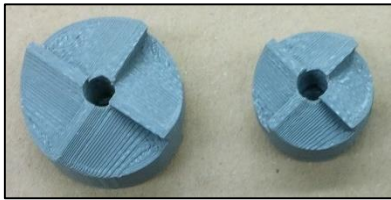


# Design: Prototype



Familiarity with general mechanics' tools

- Take concept of reverse counterbore tool used for metals and modify for current effort – fabricate from plastic

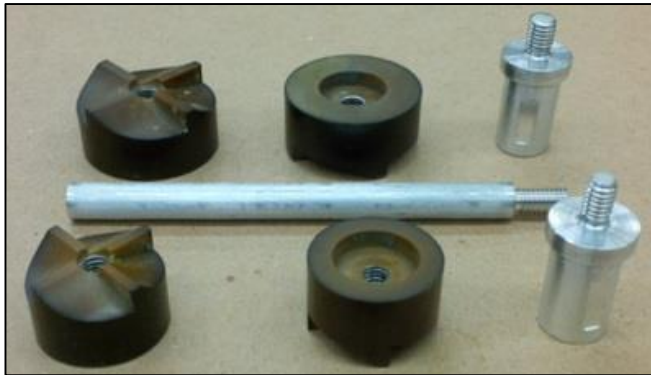


1<sup>st</sup> iteration – 3D printed cutters



Test concept – 3D printed 2 most prevalent sizes for nutplates - assessed form and fit

Transition into fabricating/machining from Torlon 5030 to fit both Andrews Tool and drill motor



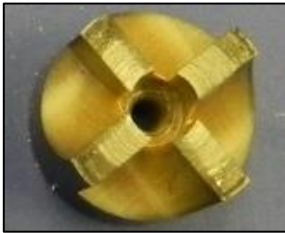


# Prototype Evolution

## Trials of Torlon 5030 machined cutters



Effectively and quickly removed (in a min or less) remnant adhesive on aluminum substructure when attached to a 1400 rpm drill motor



Thin blades – 1.91mm (0.075")  
Blade draft – 3.8mm (0.15") deep

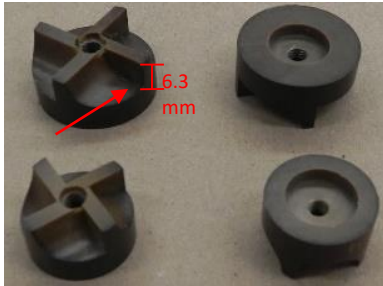
Blade edges worn away due to combination of adhesive's hardness and rotational speed of drill motor



New design for cutters needed



# Updated/Improved Cutter Design



Blade width increased to 2.84mm (0.1120")  
Draft increased to 6.35mm (0.25")

Evaluation – reran same test (w/ 1400 rpm drill motor)  
Notching of cutter blades observed where edges come in contact with adhesive



Focusing in on lower-speed models of tools  
Andrews Tool company provided 3200, 1000, and 500 rpm tools for evaluation



@ 3200 rpm – notching  
@ 1000 rpm – slight notching  
@ 500 rpm – no observed damage/wear to cutter

Selected 500 rpm Andrews Tool & 600 rpm DOTCO Drill



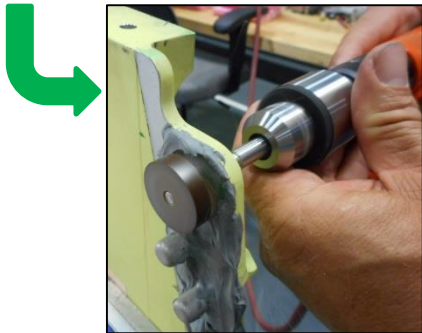
# Demonstration to Customer



Demonstration of new Torlon cutter design with 600 rpm drill motor to OEM & FSEs



Representative aircraft structure  
Failed nutplate location with  
sealant and adhesive



DOTCO pneumatic drill  
with Torlon cutter



After one min – sealant  
removed and only a  
“ghosting” of adhesive  
remaining



Surface ready  
for bonding



Abrasive pad for  
final preparation

In less < 2 min gone  
from failed nutplate to  
structure ready for  
bonding  
- Following T.O.  
procedure would have  
taken 10's of min





# Customer Evaluation



Beta kits of Torlon cutters, mandrels, and Andrews Tool Adapter

Sent to Operational units for several months of Evaluation/Field Trials

- very positive feedback – significantly reduced time for preparing structure for bonding
- found/discovered new requirements
  - additional size cutter desired – 33mm (1.3”) diameter for hard to access locations
  - difficult to remove Torlon cutters from tools
    - redesigned cutter to have a flat zone on its backside - engage with a wrench



Prototyped a wrench – field trials discovered another requirement  
- wrench needs to engage with Andrews Tool adapter

Created new prototype – field trial – customer approved new design



Worked with Custom Tool Stamping Vendor to produce for kit deployment



# Torlon Cutter

## Final Design – Build/Commercialize



Customer satisfied with Torlon cutter design now necessary to move to mass production

Optimal manufacturing method is injection molding

- reduces cost by a factor of ten
- more readily available

UDRI worked with AFC Tool Company – design of cutters for injection molding



and



Performance Plastics Ltd (PPL) for fabrication of injection mold tool & injection molding cutters



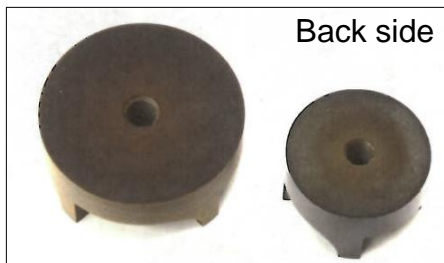
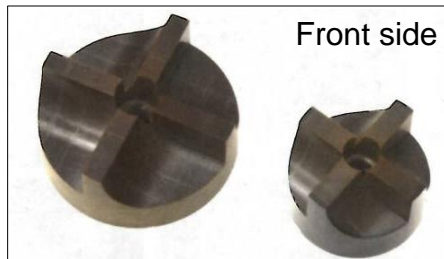


# Torlon Cutters

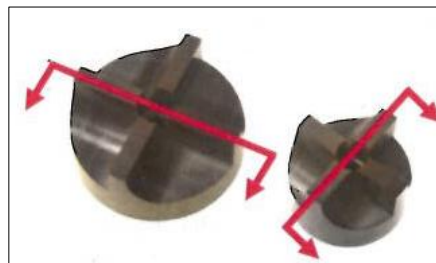
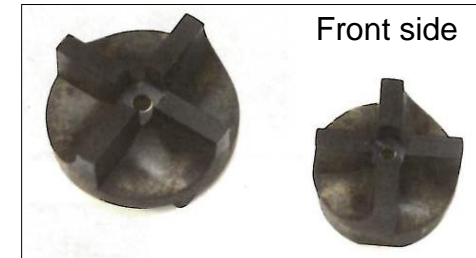
## Validation of Injection Molded Cutters

### Final Article Evaluation

Machined Cutters



Injection Molded Cutters



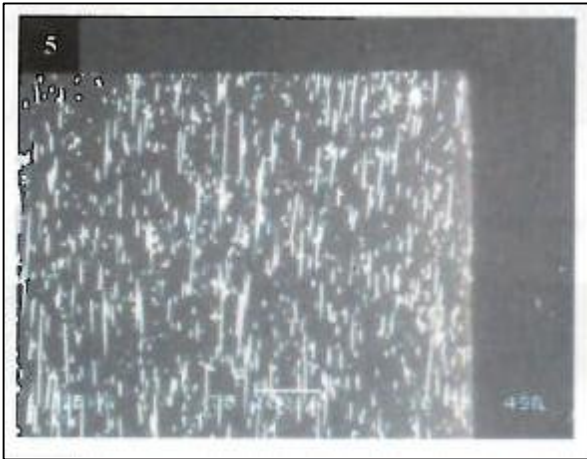
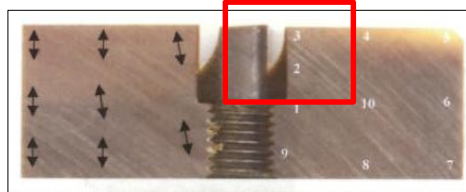
Section lines shown for photographic study



# Torlon Cutters

## Validation of Injection Molded Cutters

Representative cross-section  
through thickness of a cutter



Cutters from machined rod stock  
Fibers aligned perpendicular to cutters edge

Focusing on cutter's edge saw  
only 2% increase in fiber density  
for injection molded cutter



Injection molded cutters  
Fibers have more random orientation

Injection molded cutters subjected to hands-on evaluation

- multiple trials on test articles
- easily & efficiently removed adhesive w/o damaging structure
- performed slightly better than machined versions



# Mandrel Prototype Development



## 1<sup>st</sup> iteration

6061 Al standard mandrel  
galling observed –  
potential damage to hole



## 2<sup>nd</sup> iteration

4140 steel – shoulder added  
due to concern with FOD  
Several months in humid  
environment – pitting corrosion  
OEM concerned could cause  
damage to hole



## 3<sup>rd</sup> iteration

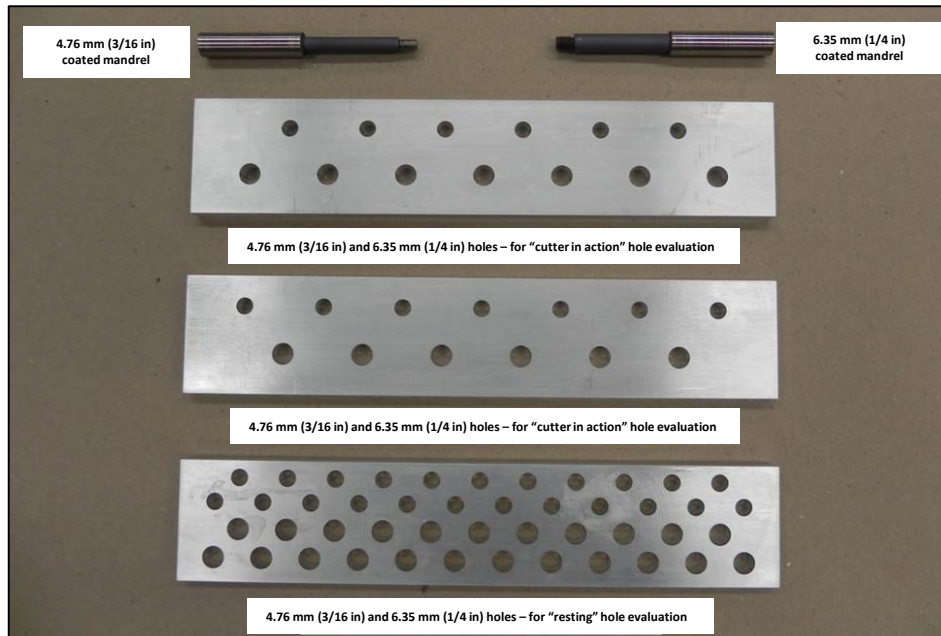
17-4 PH SS  
H-1000 condition  
Similar UTS but much  
higher corrosion resistance  
No observed corrosion after  
months of testing





# Mandrel Evaluation

Two set of 4.76mm (3/16") and 6.35mm (1/4") dia 17-4 PH SS mandrels produced  
one set coated with molybdenum disulfide dry film lube  
Spun in holes associated with nutplate fasteners of 5.46mm (0.215") and 6.99mm (0.275") dia  
Simulated aircraft structure - 2124-T8151 aluminum



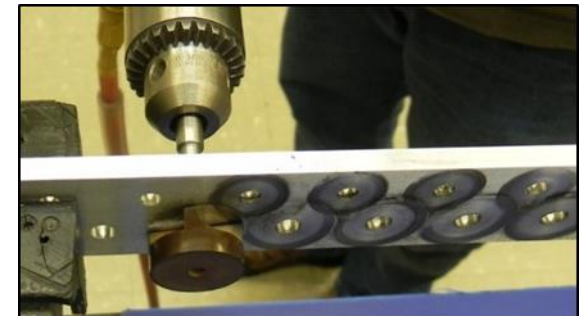
Test panels prior to mandrel evaluation



mandrel "resting" in the hole

Two conditions

mandrel simulating "cutter in action"







# Mandrel Evaluation

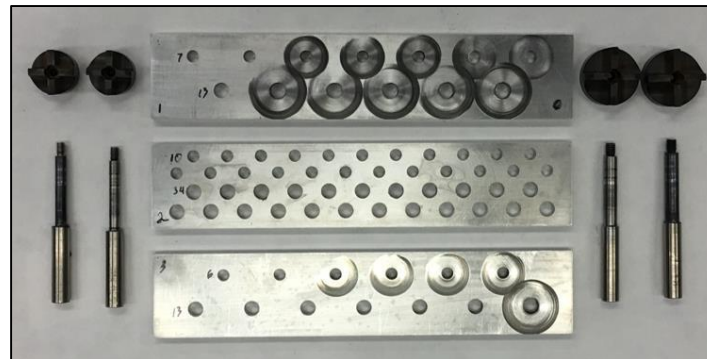
## Hole Assessment

In collaboration with OEM, two techniques employed to assess hole condition

3x Optical Microscope – topside hole



FaroArm - inside hole



## Findings

(within equipment error)

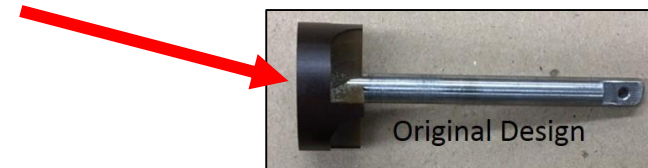
- No damage created with or without coating on mandrel
- No damage to backside of aluminum structure despite aggressiveness with cutters



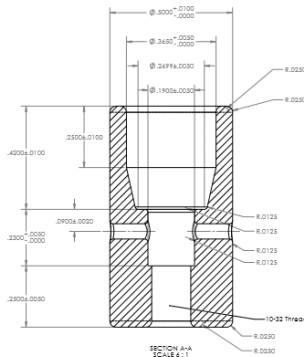
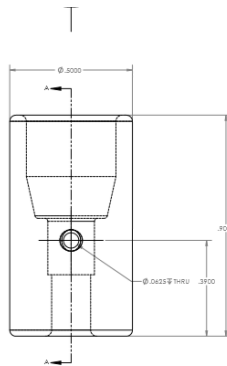
# Tetherable Mandrel Development



Feedback from maintainers' evaluation of Torlon Cutter beta kits indicated need for a swivel apparatus to attach to cutter side of mandrel



Incorporated a COTS Offshore Angle ball bearing swivel into a housing that threads onto the extended mandrel



Noble Tool Corporation manufactured two prototypes

- taken to operational units and evaluated on-aircraft
- very favorably received





# Tetherable Mandrel Development



Units desired a multi-piece (segmented) tetherable mandrel of varying lengths

- allows easier access into confined areas
- defined length of each segment

Also desired smaller (shorter) swivel connectors

AFRL/UDRI contracted Noble Tool Corp to fabricate to the new specifications



Updated swivel connector



Segmented mandrels – different diameters



Segmented tetherable mandrel broken into a tether mounting hole (a), and a 12.7mm (0.5") (b), a 63.5 (2.50"), a 38.1 (1.50") segments



Segmented tetherable mandrels with Torlon cutters & tethers



# Andrews Tool Improvements

- AFRL/UDRI discovered compressed air available for use varied across OEM & operational units
- differed from manufacturer's recommendation (lower)
  - affected efficiency of Andrews tool

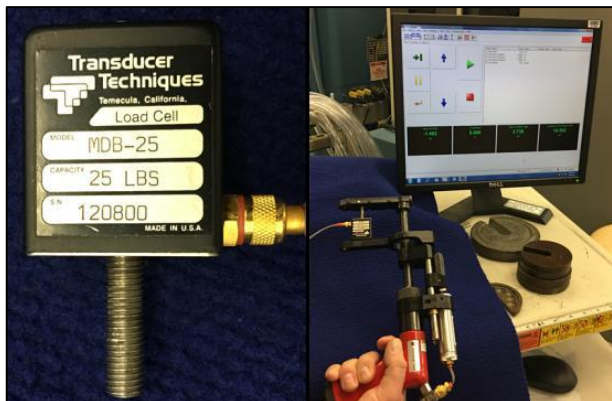
AFRL/UDRI conducted study to determine minimum compressed air pressure required to provide adequate clamping pressure

- sufficient to ensure cutting edge of Torlon cutters can remove adhesive
- if not sufficient too much adhesive remains – more abrasive pads required - increases time

In process of conducting study found inconsistencies in tool operation

- worked with Andrews Tool Corp to address

Bottom-Line: With tool improvements found that 90 psi inlet pressure to the tool (98N or 22lbs-force) is required to operate Andrews Tool efficiently



## Andrews Tool clamping force evaluation

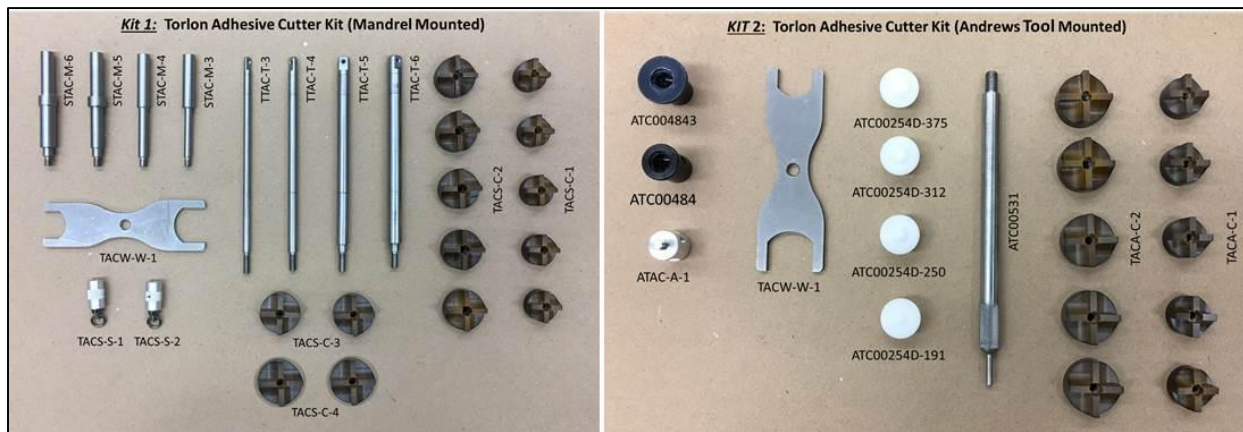
Surface Preparation Tool Force Readings (Andrews Tool Co)						
Pneumatic Tool Model # ATCP2L7-USPR500-88-R						
	Clamping Force Before Modification Newtons (lbs-force)	Clamping Force After Modification Newtons (lbs-force)	Clamping Force Before Modification Newtons (lbs-force)	Clamping Force After Modification Newtons (lbs-force)	Clamping Force Before Modification Newtons (lbs-force)	Clamping Force After Modification Newtons (lbs-force)
	621 kPa (90 psi)		687 kPa (100 psi)		758 kPa (110 psi)	
Avg of 20 cycles	85 (19)	98 (22)	107 (24)	116 (26)	116 (26)	129 (29)
Std Deviation	5.3 (1.2)	1.4 (0.32)	3.0 (0.68)	2.3 (0.51)	2.6 (0.59)	2.2 (0.50)

Note: Inlet pressure verified using a Electromatic Checkline M 3i



# Case Design

Original concept grown from initial beta kit which only included cutters, four mandrels and Andrews Tool adapters to:  
(based upon evaluation and user input which drove additional requirements)



To complete usefulness for Operational units, the Torlon cutters and their associated tools must be put into a case that is:

- durable
- allows for easy identification of kit tools and components
- conveniently organization for rapid kit inventory



# Case Design

## Prototype Torlon Adhesive Cutter Kit Configuration



Drill Motor



Andrews Tool Motor







# Case Design



- Iterative process that followed the established New Product Development Cycle utilized to evolve non-metallic reverse counterbore Torlon Adhesive Cutters from concept to a commercialized product
- Key to successful development was close working relationship between AFRL/UDRI and targeted end-users (OEM and operational unit maintainers)

Kit soon to be available

- will dramatically reduce time to remove remnant sealant/adhesive w/o damaging aircraft structure
- will result in reduction of maintenance manhours associated with repair/replacement of bonded nutplates
- will increase aircraft availability for Air Force and other services



# Acknowledgements



This work was conducted under USAF contract FA8650-11-D-5610 Task Order 0001, Project 1-040 by UDRI under direction of AFRL's Materials Integrity Branch (AFRL/RXSA). Kara Storage (RXSA) served as the contract monitor. The following provided technical advice throughout the project: Chad Hunter (AFRL/RXS); Steve Twaddle and Stuart Street (Lockheed Martin); Wayne Cox, Mike Fleischmann, Ken Hollingsworth, Don Mottor, and Beau Turner (Northrop Grumman Corporation). Tim Swigart (RXSA) performed the evaluation of the spinning mandrel's effect on fastener holes. Brad Pinnell (UDRI) performed the photomicroscopy and cross-sections. Technical advice and material support were provided by Bruce Hackett (AFC Tools); Tom Mendel, Anthony Malone, and Heidi Page (Performance Plastics Limited); and Lynn Robinson (Noble Tools). Development support was provided by provided Lucas Abrahamson and Christian Pfledderer (Southwestern Ohio Council for Higher Education).